

77 K STREET
Washington, DC

Todd Povell | Construction Management | Consultant: Dr. John Messner



APPENDIX B

Structural Slab Design

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Design calculations and tables are derived from Concrete Reinforcing Steel Institute Design Handbook, 2002.

Slab Design

Typical Bay Size: 30' x 30'

Average Column Size: 24" x 24"

Live Load: 100 PSF

Dead Load:

Ceiling.....	10 PSF
Sarnatherm XPS Insulation.....	0.69 PSF
Sarnafelt NWP-HD Separation Layer.....	0.13 PSF
Sarnafil G476-15 Waterproofing Membrane.....	0.33 PSF
Drainage Panel 900.....	0.23 PSF
Saturated Growth Media and Plants.....	48 PSF
	<u>59.38 PSF</u> \approx 60 PSF

Strength Design

$$w_u = 1.4 \text{ Dead Load} + 1.7 \text{ Live Load}$$

$$w_u = 1.4 (60 \text{ PSF}) + 1.7 (100 \text{ PSF})$$

$$w_u = 254 \text{ PSF}$$

Clear span between the column and interior beam is conservatively estimated to be 13'-6". Clear span between columns is 28'-0". Therefore the clear span between column line and interior beam is likely even smaller than 13'-6" given that the beam design will likely yield a beam width of greater than 1'-0". Assuming a larger clear span value is a conservative estimate for the slab thickness design.

The minimum allowable slab thickness is $l/28 = 15'/28 = 6.4"$. Therefore, a minimum slab thickness of 6.5" will be used.

Based on the Solid One-Way Slab tables in Chapter 7 of the CRSI Handbook, the minimum amount of reinforcement that can be used in a 6.5" slab based on a factored load of 254 PSF is $\rho \approx 0.0050$. End span and interior span tables located on pages 7-12 and 7-17, respectively, are used. End span loading is most critical in determining slab thickness because of the increased shear in these regions.

End Spans: See Table 1.

$$w_u = 312 \text{ PSF capacity} > 254 \text{ PSF}$$

Top Bars, #5 @ 11"

Bottom Bars, #5 @ 12"

Top Bars at Free End, #4 @ 12"

Temperature Bars, #4 @ 17"

Interior Spans: See Table 2.

$$w_u = 355 \text{ PSF capacity} > 254 \text{ PSF}$$



Top Bars, #5 @ 11"
 Bottom Bars, #4 @ 10"
 Temperature Bars, #4 @ 17"

Serviceability Check

1. Deflection - Maximum deflection occurs in the end span.

$$\text{Service Load} = \left(\frac{1}{1.7}\right) w_u = \left(\frac{1}{1.7}\right) (232 \text{ PSF}) = 136.5 \text{ PSF}$$

$$\begin{aligned} \text{Live Load Deflection} &= \left(\frac{L}{\text{Service}}\right) \left(\frac{l_n \times 12 \text{ in/ft}}{360}\right) < \frac{l}{360} \\ &= \left(\frac{100 \text{ PSF}}{136.5 \text{ PSF}}\right) \left(\frac{13.5' \times 12 \text{ in/ft}}{360}\right) < \frac{15'}{360} \\ &= 0.33" < 0.50" \qquad \text{OK!} \end{aligned}$$

2. Crack Control – Based on ACI 10.6.4, for 3/4" concrete cover, bar spacing is limited to 12". Bar spacing in design is satisfactory.

Beam Design

Live Load: 100 PSF

Dead Load:

Ceiling.....	10 PSF
6-1/2" Concrete Slab.....	81 PSF
Sarnatherm XPS Insulation.....	0.69 PSF
Sarnafelt NWP-HD Separation Layer.....	0.13 PSF
Sarnafil G476-15 Waterproofing Membrane.....	0.33 PSF
Drainage Panel 900.....	0.23 PSF
Saturated Growth Media and Plants.....	48 PSF
	140.38 PSF ≈ 141 PSF

Strength Design

$$\begin{aligned} w_u &= 1.4 \text{ Dead Load} \times 1.7 \text{ Live Load} \\ w_u &= 1.4 (141 \text{ PSF}) \times 1.7 (100 \text{ PSF}) \\ w_u &= 368 \text{ PSF} \end{aligned}$$

Estimate end and interior span beam stem to be b=18", h=22". It was later determined that the interior spans could be designed with a beam width of 16" and larger reinforcing steel but for consistency in formwork and constructability, the interior span beams were left with a depth of 22" and a width of 18"

$$\text{Beam Stem Estimate: } [18" \times (22"-6.5")] \left(\frac{150 \text{ PCF}}{144 \text{ in}^2/\text{ft}^2}\right) (1.4) = 407 \text{ PLF}$$

$$\begin{aligned} \text{Area Factored Load: } & 368 \text{ PSF} \times 15' = \frac{5,520 \text{ PLF}}{5,927 \text{ PLF}} \\ \text{Total Factored Load, } w_u: & \end{aligned}$$



Determine load capacity of beams. See Tables 3 and 4 for end span and interior span load capacities.

End Spans: See Table 3.

$$w_u = 6.1 \text{ k/ft capacity} > 5.9 \text{ k/ft}$$

Bottom Bars, (2) #14 [$\ell_n + 12''$]
(1) #14 [$0.875 \ell_n$]

Top Bars, (3) #14

Open Stirrups: Max Spacing at Exterior End, 195G: (19)#5: 1@2", 18@9"

Open Stirrups: Max Spacing at Interior End, 164G: (16)#4: 1@2", 15@9"

Interior Spans: See Table 4.

$$w_u = 6.1 \text{ k/ft capacity} > 5.9 \text{ k/ft}$$

Bottom Bars, (2) #10 [$\ell_n + 12''$]
(1) #10 [$0.875 \ell_n$]

Top Bars, (3) #14

Open Stirrups: Max Spacing at Each End, 164G: (16)#4: 1@2", 15@9"

Girder Design

Convert to uniform loads.

Concentrated load at center = 5.93 kips/ft (30 ft) = 177.9 kips

Estimate stem to be $b=20''$, $h=28''$.

$$[20'' \times (28''-6.5'')]\left(\frac{150 \text{ PCF}}{144 \text{ in}^2/\text{ft}^2}\right)(1.4) = 627 \text{ PLF}$$

$$\text{Concentrated load factored moment, } M = \frac{(177.9 \text{ k} \times 28')}{8} = 622.65 \text{ ft-kips}$$

$$\text{Equivalent uniform load, } w = \frac{11M}{\ell_n^2} = \frac{11(622.65' \text{ kips})}{(28')^2} = 8.74 \text{ kips/ft}$$

$$\text{Total factored uniform load (for } -M_u), w_u = 8.74 \frac{\text{kips}}{\text{ft}} + 0.63 \frac{\text{kips}}{\text{ft}} = 9.37 \frac{\text{kips}}{\text{ft}}$$

$$\text{Factored positive moment, } +M_u = 622.5 \text{ ft-kips} + \frac{0.63 \text{ PLF} (28')^2}{16} = 653.4 \text{ ft-kips}$$

$$\text{Equivalent uniform load (for } +M_u), w_u = \frac{16(622.65' \text{ kips})}{(28')^2} + 0.63 \frac{\text{kips}}{\text{ft}} = 13.3 \frac{\text{kips}}{\text{ft}}$$

77 K STREET

Washington, DC

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Determine load capacity of girders. See Tables 5 and 6 for end span and interior span load capacities.

End Spans: See Table 5.

$$w_u = 9.8 \text{ k/ft capacity} > 9.37 \text{ k/ft}$$

Bottom Bars, (3) #11 [$\ell_n + 12''$]

(2) #11 [$0.875 \ell_n$]

Top Bars, (4) #12

Open Stirrups: Max Spacing at Exterior End, 175FfI: (17)#5: 1@2", 6@8", 10@11"

Open Stirrups: Max Spacing at Interior End, 155FeI: (15)#5: 1@2", 5@8", 9@11"

Interior Spans: See Table 6.

$$w_u = 10.9 \text{ k/ft capacity} > 9.37 \text{ k/ft}$$

Bottom Bars, (2) #14 [$\ell_n + 12''$]

(1) #14 [$0.875 \ell_n$]

Top Bars, (4) #14

Open Stirrups: Max Spacing at Each End, 155FeI: (15)#5: 1@2", 5@8", 9@11"

Check Torsion.

Torsional moment capacity (with open stirrups) = 15 ft-kips.

Estimate T_u for the girder with live load on one side only.

$$w_u \text{ (live load)} = 0.17 \text{ KLF (15')} = 2.55 \text{ kips/ft}$$

$$T_u = 1/11 \times (2.55 \text{ kips/ft})(30'-1.67')^2 = 186.1 \text{ ft-kips}$$

$$T_u \text{ in girder} = (60/1820)(186.1 \text{ ft-kips}) = 6.13 \text{ ft-kips} < 15$$

Closed stirrups and additional longitudinal bars are not required.

Check Shear.

$$\text{Max } V = (177.9 \text{ kips}/2) + (0.63 \text{ KLF} \times 14') = 97.8 \text{ kips}$$

$$\text{Equivalent } w_u \text{ for shear} = 97.8 \text{ kips} / 14' = 7.0 \text{ kips/ft}$$

Initial stirrup spacing is ok.

Bottom Bar Check.

$$\text{Equivalent } w_u = 13.3 \text{ kips/ft}$$

$$+M_u = 653.4 \text{ ft-kips}$$

For a 20" x 28" girder with a clear span of 28'-0" and (5)#11 bars, $+M_u = 696 \text{ ft-kips}$. OK!

Initial Stirrup Adjustment.

Adjust for equivalent w_u of 7.0 kips/ft over the full span. Based on Table 5, use stirrup spacing 155I, (15)#5's: 1@2", 14@11" at each end.

77 K STREET

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SOLID ONE-WAY SLABS—END SPAN												Top Steel for $-M_u$			
$f'_c = 3,000$ psi												$\rho \approx 0.0050$			
Grade 60 Bars															
Thickness (in.)	4	4½	5	5½	6	6½	7	7½	8	8½	9	9½	10		
Top Bars Spacing (in.)	#4	#4	#4	#4	#5	#5	#5	#5	#5	#6	#6	#6	#6		
Bottom Bars Spacing (in.)	#4	#4	#4	#4	#4	#5	#5	#5	#5	#5	#6	#6	#6		
Top Bars Free End Spacing (in.)	#4	#4	#4	#4	#4	#4	#4	#4	#4	#4	#4	#4	#4		
T-S Bars Spacing (in.)	#3	#3	#3	#3	#4	#4	#4	#4	#4	#4	#4	#5	#5		
Areas of Steel (in. ² /ft)															
Top Interior Bottom	.200	.200	.218	.267	.310	.338	.372	.377	.413	.440	.480	.528	.528		
Slab Wt. (psf)	50	56	63	69	75	81	88	94	100	106	113	119	125		

CLEAR SPAN												FACTORED USABLE SUPERIMPOSED LOAD (psf)			
6'-0"	700	906													
6'-6"	586	761	967												
7'-0"	496	645	821												
7'-6"	423	552	704	988											
8'-0"	363	475	608	856	986										
8'-6"	314	412	528	747	861	976									
9'-0"	272	359	462	656	757	858									
9'-6"	237	314	405	579	669	759	916								
10'-0"	207	276	357	513	593	674	814	890							
10'-6"	158	191	248	364	481	591	722	790	957						
11'-0"	138	167	218	323	429	528	647	708	859	987					
11'-6"	120	146	192	287	383	473	582	636	774	890					
12'-0"	105	127	169	256	343	426	524	574	700	806	952				
12'-6"	91	111	149	228	308	383	473	518	634	731	865				
13'-0"	79	97	131	204	277	346	428	469	575	664	787	937	999		
13'-6"	68	84	115	182	249	312	388	426	523	605	719	857	914		
14'-0"	58	73	101	162	224	282	352	386	477	552	657	785	837		
14'-6"	49	62	88	145	202	256	320	351	435	505	602	721	769		
15'-0"	42	53	76	129	182	231	291	320	397	462	552	662	707		
15'-6"		45	66	115	163	209	264	291	363	423	507	610	651		
16'-0"			56	102	147	190	241	265	332	388	466	562	600		
16'-6"		48	90	132	171	219	241	304	356	429	519	554			
17'-0"		40	79	118	155	199	220	278	327	395	479	511			
17'-6"			69	105	140	181	200	255	300	363	442	473			
18'-0"			60	94	126	164	182	233	275	335	409	437			
18'-6"			51	83	113	149	165	213	253	309	378	405			
19'-0"				44	73	101	135	149	195	232	284	350	374		
19'-6"					64	90	122	135	178	213	262	324	347		
20'-0"					56	80	109	122	162	195	241	300	321		

Table 1. End Span, Slab
CRSI, Page 7-12

SOLID ONE-WAY SLABS—INTERIOR SPAN												Top Steel for $-M_u$			
$f'_c = 3,000$ psi												$\rho \approx 0.0050$			
Grade 60 Bars															
Thickness (in.)	4	4½	5	5½	6	6½	7	7½	8	8½	9	9½	10		
Top Bars Spacing (in.)	#4	#4	#4	#4	#5	#5	#5	#5	#5	#6	#6	#6	#6		
Bottom Bars Spacing (in.)	#3	#3	#3	#4	#4	#4	#4	#4	#4	#5	#5	#5	#5		
T-S Bars Spacing (in.)	#3	#3	#3	#3	#4	#4	#4	#4	#4	#4	#4	#5	#5		
Areas of Steel (in. ² /ft)															
Top Interior Bottom	.200	.218	.240	.267	.310	.338	.372	.372	.413	.440	.480	.528	.528		
Slab Wt. (psf)	50	56	63	69	75	81	88	94	100	106	113	119	125		

CLEAR SPAN												FACTORED USABLE SUPERIMPOSED LOAD (psf)			
6'-0"	703	923													
6'-6"	589	775													
7'-0"	498	657	907												
7'-6"	425	562	778	988											
8'-0"	365	485	673	856											
8'-6"	315	420	586	747	935										
9'-0"	273	367	513	656	822										
9'-6"	238	321	452	579	727	894	980								
10'-0"	208	282	399	513	646	795	872								
10'-6"	181	243	317	410	539	661	779	882							
11'-0"	159	214	281	365	482	592	699	792	964						
11'-6"	139	189	249	326	432	532	629	713	870	994					
12'-0"	122	167	222	291	388	479	568	644	787	901					
12'-6"	107	148	197	261	349	433	514	583	715	819	967				
13'-0"	94	131	176	234	315	392	465	529	650	746	882				
13'-6"	82	116	157	210	285	355	423	481	593	681	806	959			
14'-0"	71	102	139	188	257	322	384	438	541	623	739	880	939		
14'-6"	61	90	124	169	233	293	350	400	495	570	678	809	863		
15'-0"	53	79	110	151	210	266	319	365	453	523	623	745	795		
15'-6"	45	69	97	136	190	242	291	333	416	480	573	688	733		
16'-0"		60	86	121	172	220	265	305	381	442	528	635	678		
16'-6"		51	76	108	156	200	242	279	350	406	487	587	627		
17'-0"			66	96	140	182	221	255	322	374	450	543	580		
17'-6"			57	86	127	165	201	233	296	345	416	503	538		
18'-0"			49	76	114	150	184	213	272	318	384	467	499		
18'-6"			42	66	102	136	167	195	250	293	355	433	463		
19'-0"				58	91	123	152	178	230	270	329	402	429		
19'-6"				50	81	111	138	162	211	249	304	373	399		
20'-0"				43	72	100	125	147	194	229	281	346	370		

Table 2. Interior Span, Slab
CRSI, Page 7-17



$f'_c = 4,000$ psi
 $f_y = 60,000$ psi

RECTANGULAR BEAMS, END SPANS

TOTAL CAPACITY $U = 1.4D + 1.7L^{(3)}$

STEM	BARS ⁽¹⁾				TOTAL CAPACITY $U = 1.4D + 1.7L^{(3)}$																ϕM_n - ϕM_u		DEFL (C) (7) $\times 10^{-3}$ in.					
	h in.	b in.	BOTTOM $f_n + 12$ in.	Lay- ers (2)	TOP	SPAN, $f_n = 28$ ft				SPAN, $f_n = 30$ ft				SPAN, $f_n = 32$ ft				SPAN, $f_n = 34$ ft				(6) ft-kip						
						LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft- sq. (5)	Af sq. in.	STEEL WGT lb.	LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft- sq. (5)	Af sq. in.	STEEL WGT lb.	LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft- sq. (5)	Af sq. in.	STEEL WGT lb.	LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft- sq. (5)	Af sq. in.	STEEL WGT lb.			
22	12	12	2# 8	1	2# 8	1.7	133G	5	-	303	1.4	133G	5	-	320	1.3	133G	5	-	336	1.1	123G	5	-	350	130	968	
			2# 9	1	2#10	2.3	243E	20	0.9	375	2.0	263E	20	0.9	402	1.7	283E	20	0.9	429	1.5*	293E	20	0.9	451	130	905	
			2#11	1	3#10	3.3	163G	7	-	503	2.9*	163G	7	-	444	2.6*	163G	7	-	467	2.3*	163G	7	-	491	161	811	
			2#14	1	2#14	4.1*	244E	20	0.9	603	3.6*	264E	20	0.9	647	3.1*	284E	20	0.9	691	2.8*	294E	20	0.9	724	199	716	
	14	14	1#10	2# 9	1	3# 7	1.9	133G	7	-	360	1.7	133G	7	-	381	1.5	123G	6	-	398	1.3	123G	6	-	419	163	806
				2#10	1	3# 9	2.8	243E	26	1.0	437	2.5	263E	26	1.0	468	2.2*	283E	26	1.0	500	1.9*	293E	26	1.0	526	149	764
				2#11	1	3#11	4.1	163G	7	-	503	3.6*	163G	7	-	532	3.1*	173G	6	-	565	2.8*	173G	6	-	594	203	677
				2#14	1	4#10	4.6*	244E	26	1.0	695	4.0*	264E	26	1.0	745	3.5*	284E	26	1.0	795	3.1*	294E	26	1.0	838	236	595
	16	16	2#10	2# 9	1	3# 8	2.3	133G	8	-	398	2.0	133G	8	-	421	1.8	133G	8	-	444	1.6	133G	8	-	467	164	736
				2#11	1	3# 9	3.1	214F	32	1.1	578	2.7	234F	32	1.1	623	2.3	244F	32	1.1	657	2.1*	264F	32	1.1	702	194	677
				2#14	1	3#11	4.5*	163G	8	-	563	3.9*	163G	8	-	597	3.4*	173G	8	-	630	3.0*	173G	8	-	667	246	545
				2#10	1	3#14	5.3*	214F	32	1.1	731	4.6*	235F	32	1.1	787	4.1*	245F	32	1.1	831	3.6*	265F	32	1.1	888	240	462
	18	18	1#11	2# 8	1	3# 8	2.5	133G	10	-	424	2.2	133G	10	-	449	1.9	133G	10	-	473	1.7	123G	10	-	494	195	645
				2# 9	1	3#10	3.4	244E	39	1.3	646	3.0	264E	39	1.3	694	2.6	283E	39	1.2	742	2.3*	293E	38	1.2	791	195	603
				2#11	1	4#11	5.0	163G	10	-	892	4.4*	163G	10	-	931	3.8*	173G	10	-	970	3.4*	183G	10	-	1019	242	464
				2#14	1	3#14	6.1*	214F	39	1.3	1060	5.3*	235F	39	1.2	1119	4.7*	245F	38	1.2	1178	4.2*	265F	38	1.2	1237	351	293

Table 3. End Span, Beams
CRSI, Page 12-31

$f'_c = 4,000$ psi
 $f_y = 60,000$ psi

RECTANGULAR BEAMS, INTERIOR SPANS

TOTAL CAPACITY $U = 1.4D + 1.7L^{(3)}$

STEM	BARS ⁽¹⁾				TOTAL CAPACITY $U = 1.4D + 1.7L^{(3)}$																ϕM_n - ϕM_u		DEFL (C) (7) $\times 10^{-3}$ in.					
	h in.	b in.	BOTTOM $f_n + 12$ in.	Lay- ers (2)	TOP	SPAN, $f_n = 28$ ft				SPAN, $f_n = 30$ ft				SPAN, $f_n = 32$ ft				SPAN, $f_n = 34$ ft				(6) ft-kip						
						LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft- sq. (5)	Af sq. in.	STEEL WGT lb.	LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft- sq. (5)	Af sq. in.	STEEL WGT lb.	LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft- sq. (5)	Af sq. in.	STEEL WGT lb.	LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft- sq. (5)	Af sq. in.	STEEL WGT lb.			
22	12	12	2# 7	1	2# 9	2.1	123G	5	-	290	1.8	123G	5	-	307	1.6	123G	5	-	324	1.4	123G	5	-	342	100	516	
			2# 8	1	2#10	2.7	244E	21	0.9	367	2.3	263E	21	0.9	393	2.0	273E	20	0.9	415	1.8	283E	20	0.9	438	161	551	
			2#10	1	2#14	4.1	143G	5	-	367	3.6	143G	5	-	389	3.1	143G	5	-	412	2.8	153G	5	-	437	130	440	
			2#11	1	2#14	4.5	244E	21	0.9	558	3.9	274E	20	0.9	600	3.4	274E	20	0.9	632	3.1	283E	20	0.9	665	199	418	
	14	14	1#10	2# 8	1	3# 8	2.7	133G	7	-	354	2.3	133G	7	-	375	2.1	133G	7	-	397	1.8	133G	7	-	418	131	476
				2# 9	1	3# 9	3.3	244E	27	1.0	441	2.9	264E	26	1.0	472	2.5	284E	26	1.0	503	2.3	293E	26	1.0	521	192	473
				2#11	1	3#11	4.8	163G	7	-	441	4.2	163G	7	-	472	3.7	163G	7	-	503	3.3	173G	7	-	527	163	386
				2#10	1	4#10	5.2	244E	27	1.0	641	4.5	264E	26	1.0	689	4.0	284E	26	1.0	727	3.5	294E	26	1.0	775	236	351
	16	16	2#10	2# 8	1	3# 8	2.7	123G	8	-	352	2.4	123G	8	-	373	2.1	123G	8	-	394	1.8	123G	8	-	416	132	391
				2#10	1	3#10	4.2	214F	33	1.2	536	3.6	234F	33	1.1	579	3.2	244F	33	1.1	611	2.8	254F	32	1.1	644	194	402
				2#11	1	3#11	4.9	153G	8	-	550	4.3	153G	8	-	584	3.8	163G	8	-	623	3.3	173G	8	-	657	205	365
				2#14	1	3#14	6.6	215F	33	1.1	870	5.7	235F	33	1.1	924	5.0	245F	32	1.1	978	4.5	255F	32	1.1	1032	295	297
	18	18	1#11	2# 7	1	3# 9	3.1	123G	10	-	401	2.7	123G	10	-	426	2.4	123G	10	-	450	2.1	123G	10	-	475	151	344
				2# 8	1	3#10	4.0	244E	40	1.3	627	3.5	264E	39	1.3	675	3.1	284E	39	1.3	723	2.7	293E	39	1.3	771	242	367
				2#10	1	3#14	6.1	143G	10	-	609	5.3	143G	10	-	641	4.7	143G	10	-	673	4.2	153G	10	-	705	195	293
				2#11	1	3#14	6.5	214F	40	1.3	893	5.9	234F	39	1.3	941	5.2	244F	39	1.3	989	4.6	254F	39	1.2	1037	299	279

Table 4. Interior Span, Beams
CRSI, Page 12-61



$f'_c = 4,000 \text{ psi}$
 $f_y = 60,000 \text{ psi}$

RECTANGULAR BEAMS, END SPANS

TOTAL CAPACITY $U = 1.4D + 1.7L^{(3)}$

STEM	BARS ⁽¹⁾				TOTAL CAPACITY $U = 1.4D + 1.7L^{(3)}$																				ϕM_n $-\phi M_u$	DEFL (C)							
	h in.	b in.	BOTTOM		LAYERS (2)	TOP	SPAN, $\ell_n = 24 \text{ ft}$					SPAN, $\ell_n = 26 \text{ ft}$					SPAN, $\ell_n = 28 \text{ ft}$					SPAN, $\ell_n = 30 \text{ ft}$											
			$\ell_n + 12 \text{ in.}$	$0.875 \ell_n$			LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft-kips	Af sq. in.	STEEL WGT lb.	LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft-kips	Af sq. in.	STEEL WGT lb.	LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft-kips	Af sq. in.	STEEL WGT lb.	LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft-kips			Af sq. in.	STEEL WGT lb.	(6) ft-kip	(7) $\times 10^{-9}$ in.			
14	24	14	1	3#8	1	3.8	113I	9	-	348	3.2	123I	9	-	376	2.8	123I	6	-	399	2.4	123I	8	-	422	199	500						
						184F	35	1.3	507	4.3	134I	9	-	543	3.7	143I	9	-	523	3.7	143I	9	-	561	3.2	143I	8	-	633	234			
						185F	35	1.2	772	6.3	145I	9	-	823	5.5	154I	8	-	873	5.5	154I	8	-	873	4.8	164I	8	-	930	290			
						295C	35	1.2	1193	7.0	145I	9	-	913	6.0	165I	8	-	1063	6.0	165I	8	-	1063	5.2	165I	8	-	1119	428			
	26	14	1	3#11	1	7.4	135I	9	-	823	7.0	145I	9	-	981	6.0	165I	8	-	1063	5.2	165I	8	-	1119	428	352						
						295C	35	1.2	1283	3.15C	34	1.2	1376	2.15F	34	1.2	1244	2.15F	34	1.2	1244	2.15F	34	1.2	1244	2.15F	34	1.2	1244	2.15F	34	1.2	1244
						295C	35	1.2	1283	3.15C	34	1.2	1376	2.15F	34	1.2	1244	2.15F	34	1.2	1244	2.15F	34	1.2	1244	2.15F	34	1.2	1244	2.15F	34	1.2	1244
						295C	35	1.2	1283	3.15C	34	1.2	1376	2.15F	34	1.2	1244	2.15F	34	1.2	1244	2.15F	34	1.2	1244	2.15F	34	1.2	1244	2.15F	34	1.2	1244
	26	16	1	3#8	1	4.1	113I	11	-	395	3.5	113I	11	-	421	3.0	123I	10	-	452	2.6	123I	10	-	479	251	424						
						165G	43	1.4	657	4.9	145I	11	-	888	4.2	143I	10	-	616	3.7	143I	10	-	616	3.7	143I	10	-	700	236			
						165G	43	1.4	793	6.5	145I	11	-	827	5.6	154I	10	-	876	4.8	164I	10	-	924	4.8	164I	10	-	934	364			
						245D	43	1.4	1116	7.7	145I	11	-	1007	6.6	165I	10	-	1156	5.8	165I	10	-	1156	5.8	165I	10	-	1217	471			
26	16	2	3#14	1	9.0	145Fd	11	-	1007	7.7	145I	11	-	1068	6.6	165I	10	-	1156	5.8	165I	10	-	1156	5.8	165I	10	-	1217	301			
					245D	43	1.4	1282	265D	42	1.4	1382	265D	42	1.3	1481	265D	42	1.3	1481	265D	42	1.3	1481	265D	42	1.3	1481	265D	42	1.3	1481	
					245D	43	1.4	1282	265D	42	1.4	1382	265D	42	1.3	1481	265D	42	1.3	1481	265D	42	1.3	1481	265D	42	1.3	1481	265D	42	1.3	1481	
					245D	43	1.4	1282	265D	42	1.4	1382	265D	42	1.3	1481	265D	42	1.3	1481	265D	42	1.3	1481	265D	42	1.3	1481	265D	42	1.3	1481	
18	24	1	3#9	1	4.5	113I	13	-	410	3.9	113I	13	-	437	3.3	113I	13	-	464	2.9	123I	13	-	496	238	377							
					165G	52	1.5	682	5.5	154I	13	-	678	4.7	143I	13	-	667	4.1	143I	13	-	667	4.1	143I	13	-	707	368				
					165G	52	1.5	846	7.2	145I	13	-	1030	6.2	154I	13	-	1023	5.4	164I	13	-	1089	4.8	164I	13	-	1089	442				
					245D	52	1.5	1260	8.9	165Fd	13	-	1101	7.7	165I	13	-	1249	6.7	165I	13	-	1315	6.7	165I	13	-	1315	568				
18	24	1	3#14	1	10.5	155Fd	13	-	1101	11.3	175Fd	15	-	1486	9.8	175Fd	15	-	1573	8.5	175Fd	15	-	1673	696	268							
					295C	52	1.5	1475	265D	51	1.5	1481	265D	51	1.5	1588	265D	51	1.5	1588	265D	51	1.5	1588	265D	51	1.5	1588	265D	51	1.5	1588	
					295C	52	1.5	1475	265D	51	1.5	1481	265D	51	1.5	1588	265D	51	1.5	1588	265D	51	1.5	1588	265D	51	1.5	1588	265D	51	1.5	1588	
					295C	52	1.5	1475	265D	51	1.5	1481	265D	51	1.5	1588	265D	51	1.5	1588	265D	51	1.5	1588	265D	51	1.5	1588	265D	51	1.5	1588	
20	24	1	3#9	1	5.2	113I	15	-	463	4.4	113I	15	-	495	3.8	123I	15	-	531	3.3	123I	15	-	562	298	345							
					159H	61	1.7	724	6.0	165H	61	1.7	777	5.2	143I	15	-	729	4.5	143I	15	-	729	4.5	143I	15	-	773	371				
					134I	15	-	684	9.1	155Fd	15	-	1173	7.8	155I	15	-	1240	6.8	165I	15	-	1321	6.8	165I	15	-	1321	576				
					215E	61	1.7	1015	11.3	175Fd	15	-	1486	10.9	175Fd	15	-	1573	9.5	175Fd	15	-	1673	9.5	175Fd	15	-	1673	612				
20	24	1	3#14	1	10.6	145Fd	15	-	1067	11.3	175Fd	15	-	1486	10.9	175Fd	15	-	1573	9.5	175Fd	15	-	1673	696	219							
					295C	61	1.7	1485	11.3	175Fd	15	-	1486	10.9	175Fd	15	-	1573	9.5	175Fd	15	-	1673	9.5	175Fd	15	-	1673	696				
					295C	61	1.7	1485	11.3	175Fd	15	-	1486	10.9	175Fd	15	-	1573	9.5	175Fd	15	-	1673	9.5	175Fd	15	-	1673	696				
					295C	61	1.7	1485	11.3	175Fd	15	-	1486	10.9	175Fd	15	-	1573	9.5	175Fd	15	-	1673	9.5	175Fd	15	-	1673	696				
20	24	1	4#14	1	13.3	295C	61	1.7	2156	12.6	315C	61	1.7	1888	10.9	345C	60	1.6	2037	9.5	365C	59	1.6	1695	602	219							
					485A	61	1.7	2156	12.6	315C	61	1.7	1888	10.9	345C	60	1.6	2037	9.5	365C	59	1.6	1695	602	219								
					485A	61	1.7	2156	12.6	315C	61	1.7	1888	10.9	345C	60	1.6	2037	9.5	365C	59	1.6	1695	602	219								
					485A	61	1.7	2156	12.6	315C	61	1.7	1888	10.9	345C	60	1.6	2037	9.5	365C	59	1.6	1695	602	219								

Table 5. End Span, Girder
CRSI, Page 12-34

$f'_c = 4,000 \text{ psi}$
 $f_y = 60,000 \text{ psi}$

RECTANGULAR BEAMS, INTERIOR SPANS

TOTAL CAPACITY $U = 1.4D + 1.7L^{(3)}$

STEM	BARS ⁽¹⁾				TOTAL CAPACITY $U = 1.4D + 1.7L^{(3)}$																				ϕM_n $-\phi M_u$	DEFL (C)							
	h in.	b in.	BOTTOM		LAYERS (2)	TOP	SPAN, $\ell_n = 24 \text{ ft}$					SPAN, $\ell_n = 26 \text{ ft}$					SPAN, $\ell_n = 28 \text{ ft}$					SPAN, $\ell_n = 30 \text{ ft}$											
			$\ell_n + 12 \text{ in.}$	$0.875 \ell_n$			LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft-kips	Af sq. in.	STEEL WGT lb.	LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft-kips	Af sq. in.	STEEL WGT lb.	LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft-kips	Af sq. in.	STEEL WGT lb.	LOAD (4) k/ft	STIR TIES (5)	ϕT_n ft-kips			Af sq. in.	STEEL WGT lb.	(6) ft-kip	(7) $\times 10^{-9}$ in.			
14	24	14	1	3#8	1	5.5	113I	9	-	381	4.7	113I	9	-	408	4.1	123I	9	-	439	3.5	123I	9	-	467	199	287						
						185F	35	1.3	671	5.8	124I	9	-	522	5.0	134I	9	-	599	5.0	134I	9	-	599	4.4	133I	9	-	679	290			
						185F	35	1.3	760	7.5	135I	9	-	789	6.5	144I	9	-	778	5.6	144I	9	-	778	5.6	144I	9	-	825	359			
						295C	35	1.3	1112	9.3	145Fd	9	-	996	8.1	145I	9	-	1059	7.0	155I	9	-	1059	7.0	155I	9	-	1134	411			
	26	14	1	3#14	1	11.0	264C	9	-	967	9.3	145Fd	9	-	996	8.1	145I	9	-	1059	7.0	155I	9	-	1059	7.0	155I	9	-	1134	411		
						295C	35	1.3	1294	3.15C	35	1.2	1393	3.45C	34	1.2	1510	3.65C	34	1.2	1609	3.65C	34	1.2	1609	3.65C	34	1.2	1609	3.65C	34	1.2	1609
						295C	35	1.3	1294	3.15C	35	1.2	1393	3.45C	34	1.2	1510	3.65C	34	1.2	1609	3.65C	34	1.2	1609	3.65C	34	1.2	1609	3.65C	34	1.2	1609
						295C	35	1.3	1294	3.15C	35	1.2	1393	3.45C	34	1.2	1510																